

Hanbury
Brown-Twiss
(HBT)
interferometry
with
event-by-event
fluctuations

Christopher J.
Plumberg
In
collaboration
with Chun
Shen and
Ulrich Heinz
(arXiv:1306.1485)

Hanbury Brown-Twiss (HBT) interferometry with event-by-event fluctuations

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The Ohio State University

March 8, 2014

Background and Motivation

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Hanbury-Brown–Twiss (HBT) interferometry (also, 'intensity interferometry' or 'femtoscopy') relies on two-particle momentum correlations to study the geometric and flow properties of heavy-ion collisions:

- azimuthally-sensitive HBT analyses communicate important information about deformations in the structure of the freeze-out surface
- odd harmonics present in HBT radii known to open the window to the study of event-by-event fluctuations
- fulfills a vital role in constraining the initial state of the fireball and its subsequent evolution

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Part 1: 3rd order HBT

HBT Basics

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Two particles: $\vec{p}_1, \vec{p}_2 \longrightarrow \vec{q} \equiv \vec{p}_1 - \vec{p}_2, \vec{K} \equiv \frac{1}{2}(\vec{p}_1 + \vec{p}_2)$

Correlation function: $C(\vec{p}_1, \vec{p}_2) \equiv \frac{E_{p_1} E_{p_2} \frac{dN}{d^3 p_1 d^3 p_2}}{\left(E_{p_1} \frac{dN}{d^3 p_1}\right) \left(E_{p_2} \frac{dN}{d^3 p_2}\right)}$

Ignoring final-state interactions, C may be fit to the form:

$$C(\vec{q}, \vec{K}) = 1 \pm \lambda(\vec{K}) \exp \left(- \sum_{i,j=o,s,l} R_{ij}^2(\vec{K}) q_i q_j \right),$$

$R_{ij}^2 = R_{ij}^2(|\vec{K}|, \Phi_K) \rightarrow$ measure Φ_K with respect to what?

Fourier moments of $R_{ij}^2(\vec{K})$

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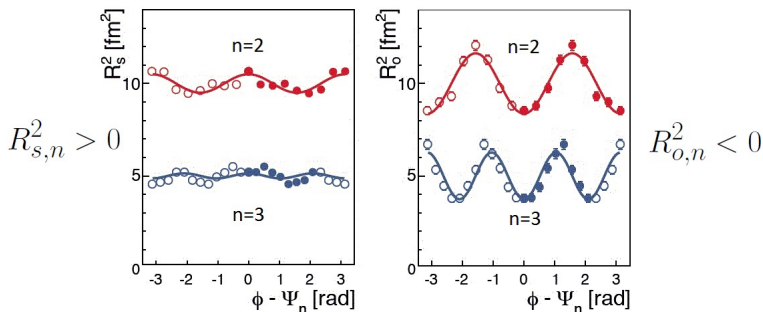
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- Experimentally, one measures HBT correlations as a function of the *difference* between Φ_K and one of the flow angles Ψ_n
 \Rightarrow we plot observable quantities against $\Phi_K - \Psi_n$,
($n = 1, 2, 3, \dots$)
- The flow angle is defined by Ψ_n in $v_n e^{in\Psi_n} \equiv \langle e^{in\phi_p} \rangle$
- The v_n are the anisotropic flow coefficients and ϕ_p is the azimuthal angle of \vec{p}_T of the emitted particles in the lab frame
- \Rightarrow Fourier-decompose the R_{ij}^2 :

$$\begin{aligned} R_{ij}^2(|\vec{K}|, \Phi_K) &= 2 \sum_{n=1}^{\infty} \left(R_{ij,n}^{2(c)}(|\vec{K}|) \cos[n(\Phi_K - \Psi_n)] \right. \\ &\quad \left. + R_{ij,n}^{2(s)}(|\vec{K}|) \sin[n(\Phi_K - \Psi_n)] \right) + R_{ij,0}^2(|\vec{K}|) \end{aligned}$$

PHENIX data

T. Niida, (QM 2012, arXiv:1304.2876) (integrated over K_{\perp})



Important features to understand:

- Different signs of Fourier coefficients in out and side directions
- Different oscillation amplitudes: $R_{o,n}^2/R_{s,n}^2 \gg 1$

Emission function

We define the emission function $S(x, K)$ as the Wigner density of the fireball

$$\text{Emission function: } \int d^4x S(x, K) = E_K \frac{dN}{d^3K}$$

Taking $\lambda(\vec{K}) = 1$, C and S may be related by

$$C(\vec{q}, \vec{K}) \approx 1 + \left| \frac{\int d^4x e^{iq \cdot x} S(x, K)}{\int d^4x S(x, K)} \right|^2$$

- For Gaussian sources $S(x, K)$, $R_{ij}^2 = \langle (\tilde{x}_i - \beta_i \tilde{t})(\tilde{x}_j - \beta_j \tilde{t}) \rangle$, where
- $\tilde{x}_i \equiv x_i - \langle x_i \rangle$, $\tilde{t} \equiv t - \langle t \rangle$, $\vec{\beta} \equiv \vec{K}/K^0$ and
- $\langle f(x) \rangle \equiv \frac{\int d^4x f(x) S(x, K)}{\int d^4x S(x, K)}$
 \Rightarrow given $S(x, K)$, $R_{ij}^2(\vec{K})$ may be computed directly

Emission function

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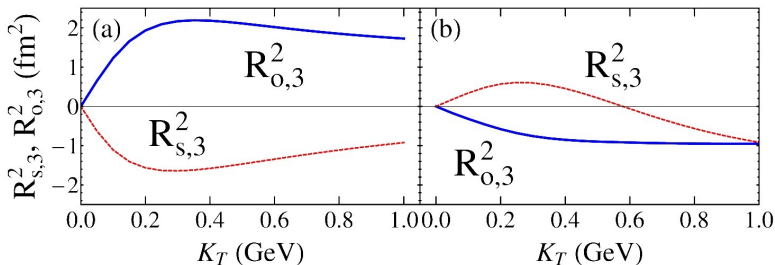
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- Consider S with two kinds of different triangular deformations:
 - "Geometric case" - Triangular spatial deformation with radial flow, no triangular flow
 - "Flow case" - Triangular flow, no spatial deformation
- Can obtain triangular oscillations of R_{ij}^2 from
 - triangular flow deformation
 - triangular spatial deformation coupled to radial flow
 - combinations thereof

HBT oscillation amplitudes: two examples

Geometric case

Flow case



Part 1: Conclusions

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- Without radial flow, a triangular spatial deformation of the source at freeze-out leaves no measurable trace in the HBT radii oscillations
- Triangular oscillations of HBT radii may generally result from an admixture of triangular collective flow *and* triangular spatial deformation coupling to radially symmetric flow
- We can distinguish "flow domination" from "geometry domination" by the phases and K_T -dependence of the respective oscillation amplitudes; PHENIX data appear to point to "flow domination"

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Part 2:

Event-by-event hydrodynamics

Next steps...

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- Our analysis assumed Gaussian, ensemble-averaged ansatz for $S(x, K)$
 \Rightarrow *what do we find in an event-by-event (EBE) hydrodynamic treatment?*
- Construct (viscous) hydrodynamic emission function using Cooper-Frye formula:

$$\begin{aligned} S_{\text{hydro}}(x, K) &= \frac{1}{(2\pi)^3} \int_{\Sigma(x_f)} K \cdot d^3\sigma(x_f) \delta^4(x - x_f) f(x_f, K), \\ f(x, K) &= f_0 + \delta f \\ &= \frac{1}{e^{(K \cdot u - \mu)/T} \pm 1} + \frac{\chi(K^2) K^\mu K^\nu \pi_{\mu\nu}}{2T^2(e + p)} f_0 (1 \pm f_0) \end{aligned}$$

■

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- How are our results affected by ensemble-averaging?

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- How are our results affected by ensemble-averaging?
- How should one extract HBT radii from a non-Gaussian source?

(At least) 3 Ways of getting HBT radii

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- Option 1: compute R_{ij}^2 from S_{hydro} via source variances,

$$R_{ij}^2 = \langle (\tilde{x}_i - \beta_i \tilde{t})(\tilde{x}_j - \beta_j \tilde{t}) \rangle = -\frac{1}{2(C-1)} \left. \frac{\partial^2 C}{\partial q_i \partial q_j} \right|_{q \rightarrow 0}$$

- Option 2: Construct $C(q, K)$ from $S_{hydro} \rightarrow$ extract R_{ij}^2 from Gaussian fit to correlator,
 $C - 1 \sim \exp \left(- \sum_{i,j} R_{ij}^2 q_i q_j \right)$
- Option 3: Construct $C(q, K)$ from $S_{hydro} \rightarrow$ extract R_{ij}^2 from "q-moments method":

$$\frac{1}{2} (\mathcal{R}^{-1})_{ij} = \frac{\int d^3 q q_i q_j (C - 1)}{\int d^3 q (C - 1)}, \quad \text{where } \mathcal{R} \equiv (R_{ij}^2) (K)$$

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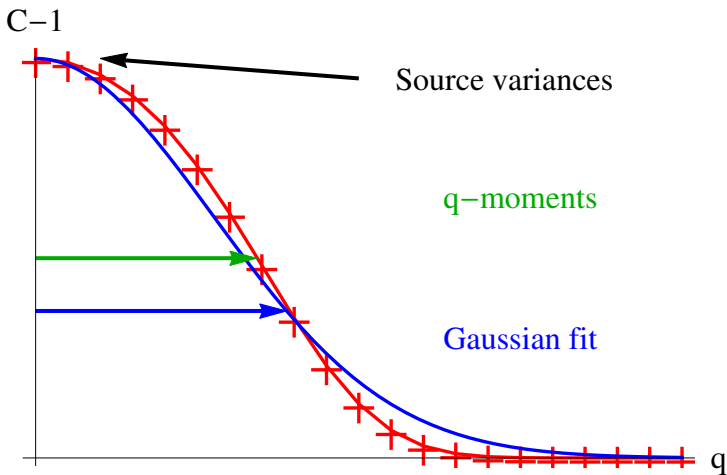
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Comparison of HBT methods

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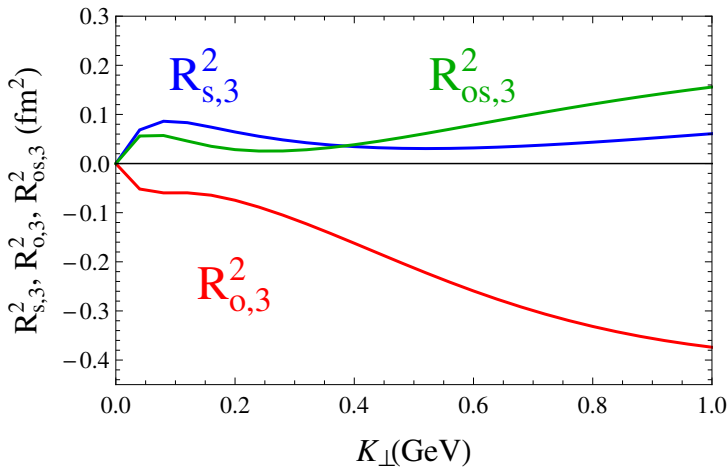
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Results

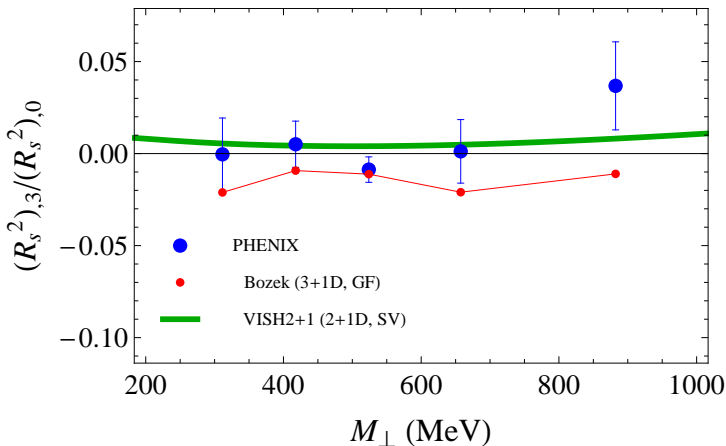
Hydrodynamic approach

K_{\perp} -dependence of $R_{ij,3}^2$ from hydrodynamics



Hydrodynamic approach

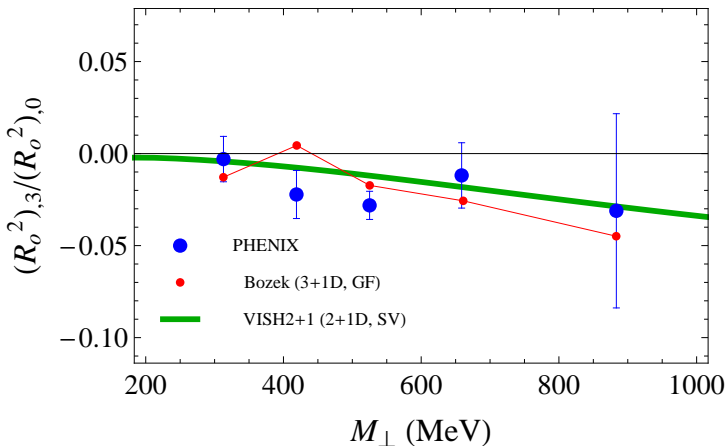
M_{\perp} -dependence of $R_{s,3}^2/R_{s,0}^2$ from hydrodynamics¹



¹arXiv:1401.7680, arXiv:1401.4894

Hydrodynamic approach

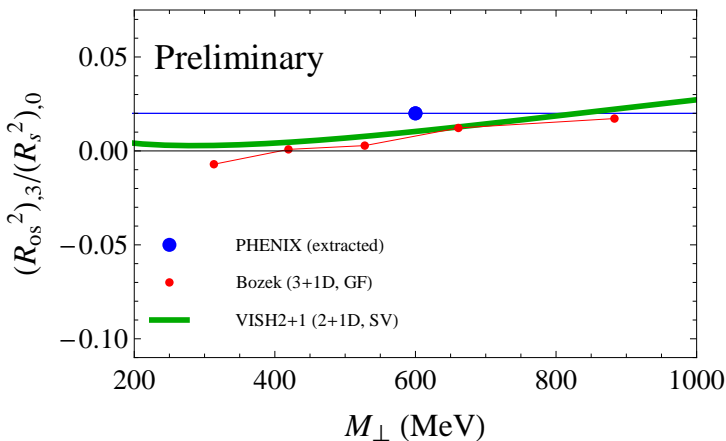
M_{\perp} -dependence of $R_{o,3}^2/R_{o,0}^2$ from hydrodynamics²



²arXiv:1401.7680, arXiv:1401.4894

Hydrodynamic approach

M_{\perp} -dependence of $R_{os,3}^2/R_{s,0}^2$ from hydrodynamics³



³arXiv:1401.7680, arXiv:1401.4894

Part 2: Conclusions

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- VISH2+1 qualitatively reproduces general trends of PHENIX data
- Qualitative features of K_{\perp} -dependence of hydrodynamic $R_{ij,3}^2$ similar to toy model for small K_{\perp} , more discrepancies at $K_{\perp} \gtrsim 0.3$ GeV
- Subtleties involving ensemble-averaging and the construction of the correlation function have not been addressed here

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Thanks also to my collaborators

Ulrich Heinz and Chun Shen!

Double-Fourier formalism

Define

$$S_{\ell,m} \equiv e^{-im\psi_3} \int_{-\pi}^{\pi} \frac{d\phi}{2\pi} e^{i\ell\phi} \int_{-\pi}^{\pi} \frac{d\Phi_K}{2\pi} e^{im\Phi_K} S(\phi, \Phi_K),$$

$$\longrightarrow \mathcal{Z}_{\ell} \equiv e^{-i\ell\psi_3} \sum_{m=-\infty}^{\infty} S_{\ell,m-\ell} e^{-im(\Phi_K - \psi_3)} \equiv \mathcal{X}_{\ell} + i\mathcal{Y}_{\ell}$$

We can show, e.g.,

$$\langle x_s^2 \rangle = \int_{-\infty}^{\infty} d\eta \int_0^{\infty} \tau d\tau \int_0^{\infty} r dr \pi r^2 (\mathcal{X}_0 - \mathcal{X}_2)$$

$$\langle x_s \rangle = \int_{-\infty}^{\infty} d\eta \int_0^{\infty} \tau d\tau \int_0^{\infty} r dr 2\pi r \mathcal{Y}_1$$

- Since $R_s^2 = \langle x_s^2 \rangle - \langle x_s \rangle^2$, no dependence on $\ell \geq 3$ (similarly for other R_{ij}^2)!
- N.B.: same expression contains all orders in Φ_K

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Toy model for the source

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$$S(x, K) = \frac{S_0(K)}{\tau} \exp \left[-\frac{(\tau - \tau_f)^2}{2\Delta\tau^2} - \frac{(\eta - \eta_0)^2}{2\Delta\eta^2} \right. \\ \left. - \frac{r^2}{2R^2} (1 + 2\bar{\epsilon}_3 \cos(3(\phi - \bar{\psi}_3))) \right. \\ \left. - \frac{M_\perp}{T_0} \cosh(\eta - Y) \cosh \eta_t + \frac{K_\perp}{T_0} \cos(\phi - \Phi_K) \sinh \eta_t \right]$$

where

$$\eta_t = \frac{\eta_f r}{R} (1 + 2\bar{v}_3 \cos(3(\phi - \bar{\psi}_3)))$$

- $\bar{\epsilon}_3$: triangular azimuthal deformation
- \bar{v}_3 : triangular flow deformation
- η_f : collective radial flow rapidity
- $\bar{\psi}_3$: triangular flow velocity angle, points in direction of largest flow rapidity and steepest descent of spatial density profile (note: $\Psi_n \neq \bar{\psi}_n$ in general)